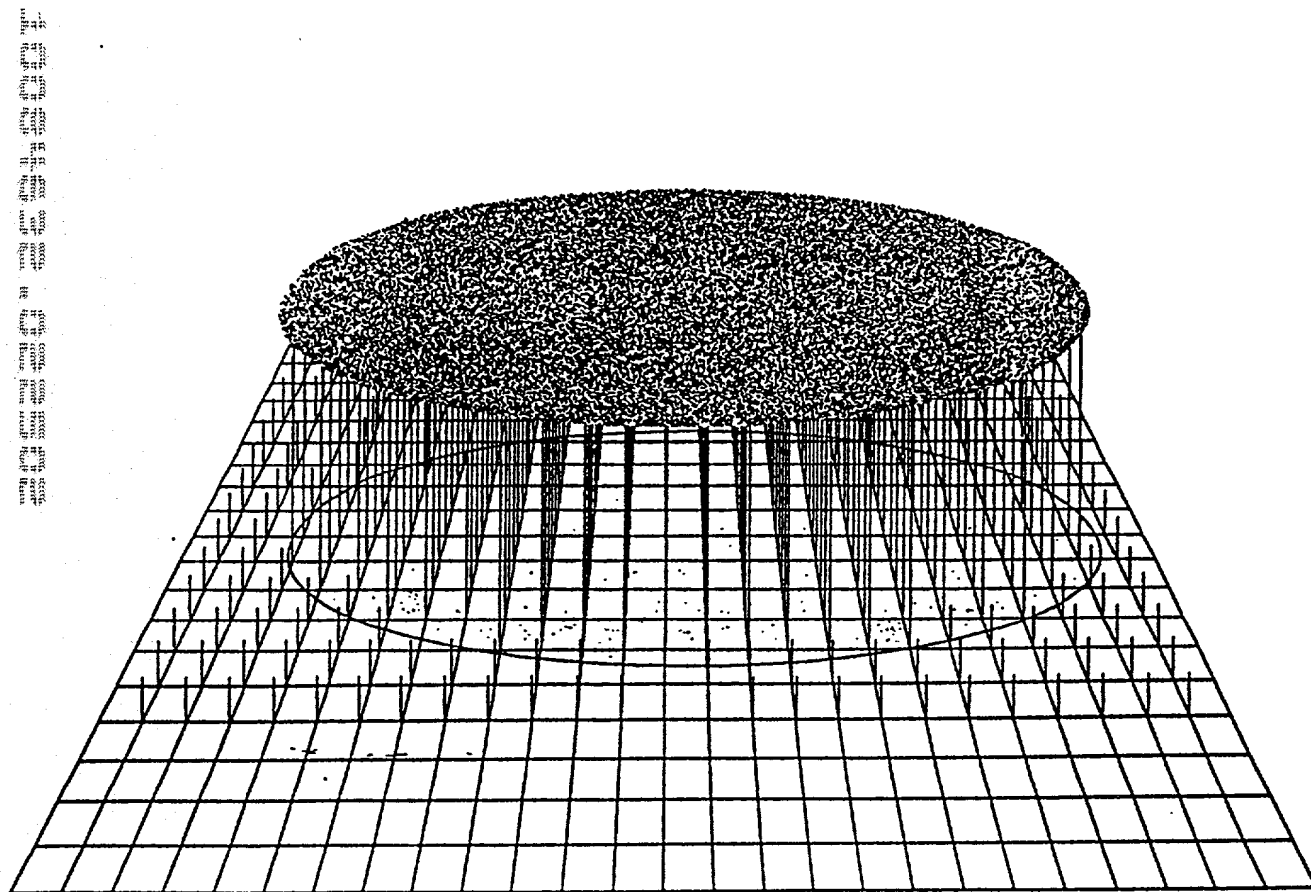


Standard Immunoassay Use

Determination of mass per unit volume (eg. ng/ml) or equivalent (eg. IU)

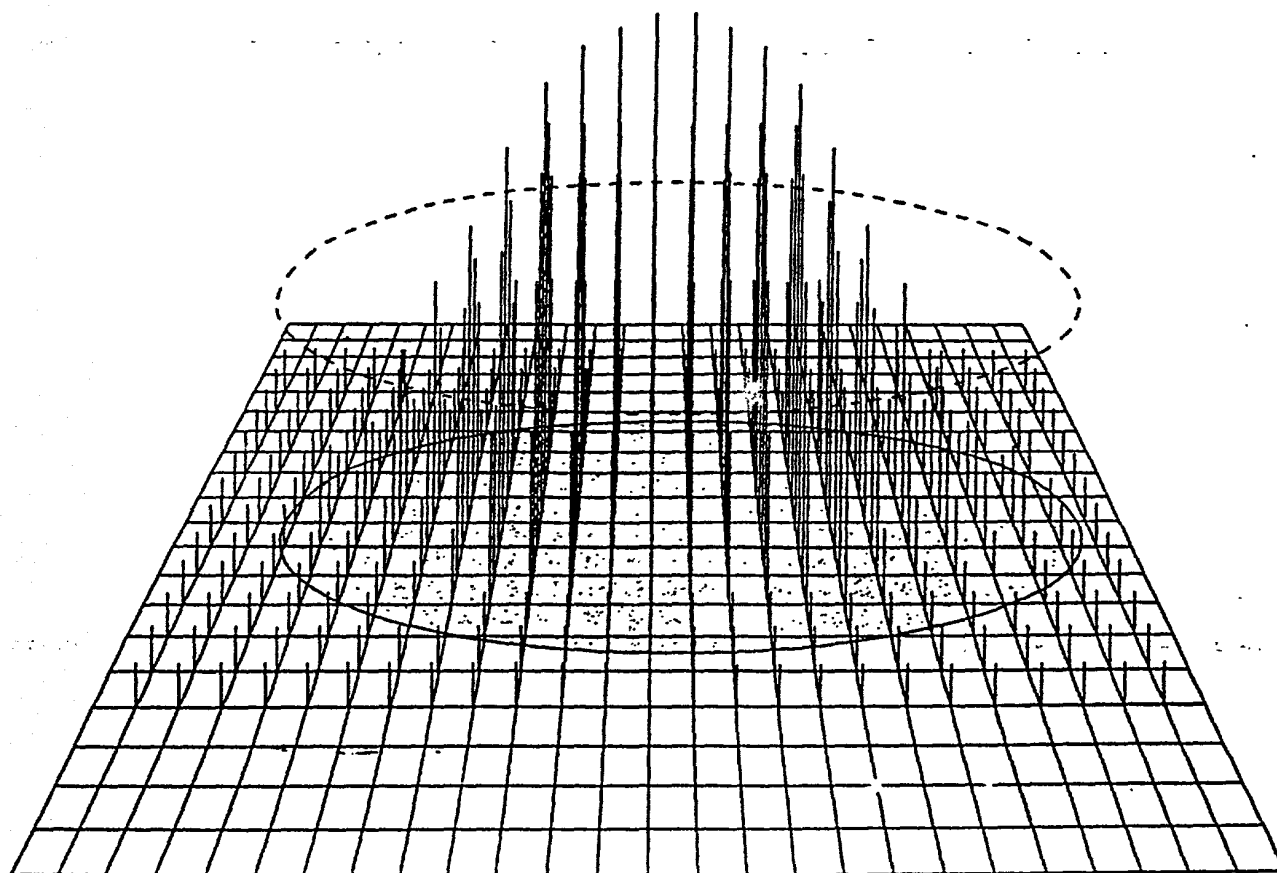


The effect of the use of a single large beam (in this case approx. 2mm) for reading the surface is the production of a single result representing the mass change effects of all binding events within the spot area.

Figure 1

Standard Immunoassay Use

Determination of mass per unit volume (eg. ng/ml) or equivalent (eg. IU)

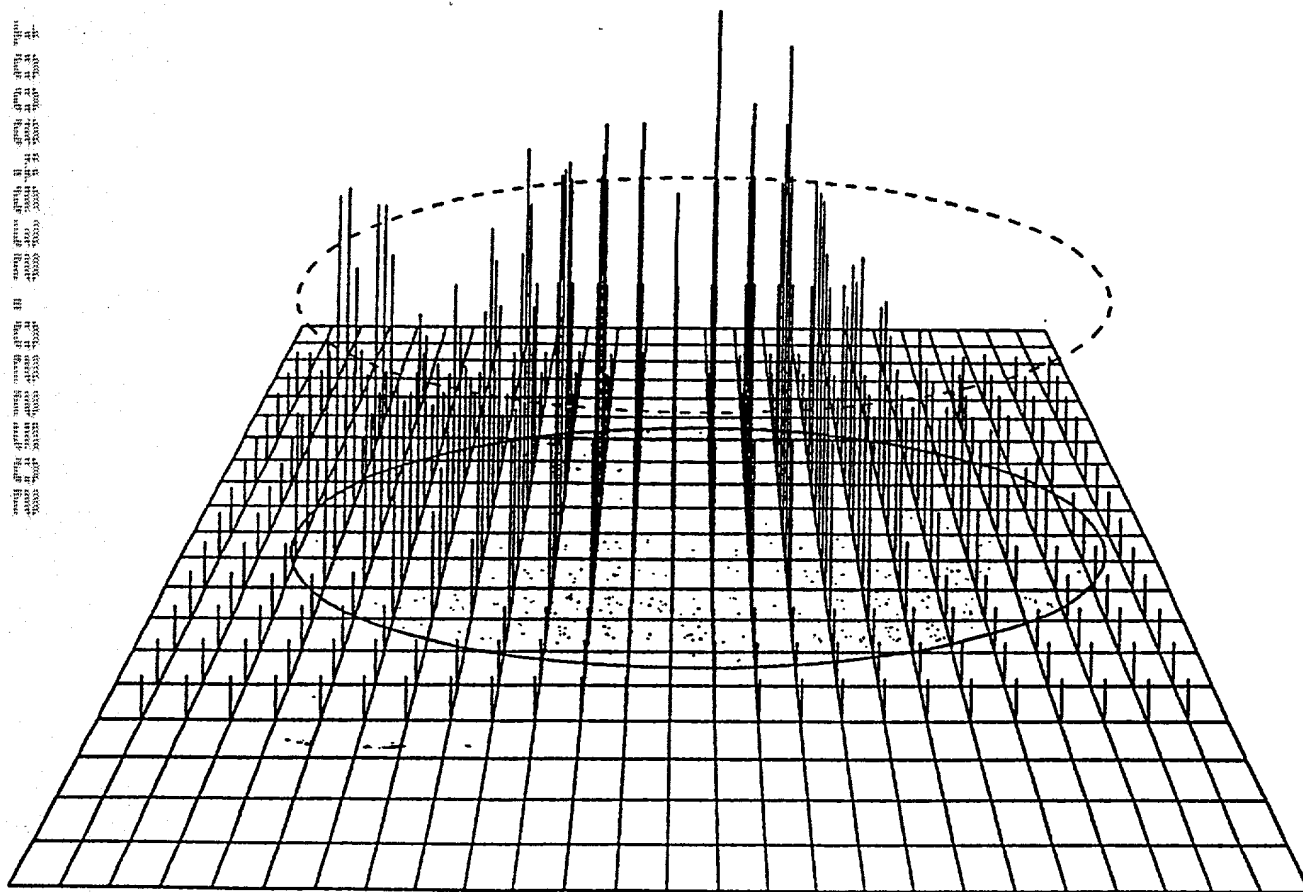


The idealized model for this method is the optical averaging occurring over the entire read area (in this case represented by an approx. normal distribution of binding events over the spot area).

Figure 2

Standard Immunoassay Use

Determination of mass per unit volume (eg. ng/ml) or equivalent (eg. IU)

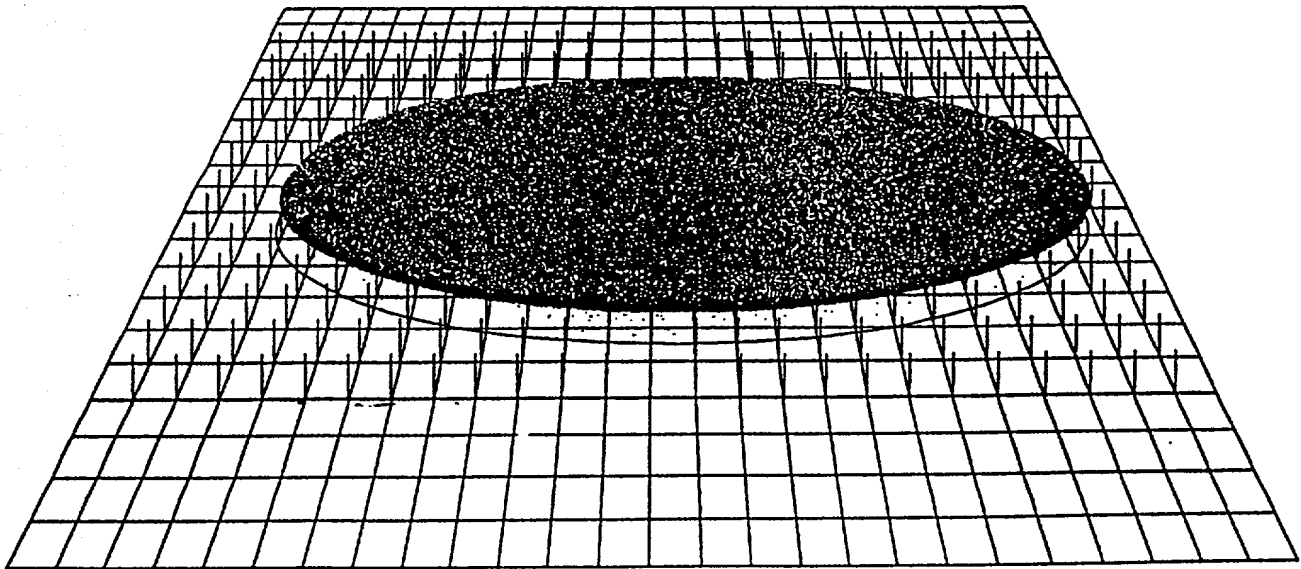


In virtually all cases the binding distribution over the spot area is actually highly inhomogeneous. The advantage of this method is that it inherently integrates all of the binding events within the spot area, without regard to their distribution.

Figure 3

Standard Immunoassay Use

Determination of mass per unit volume (eg. ng/ml) or equivalent (eg. IU)

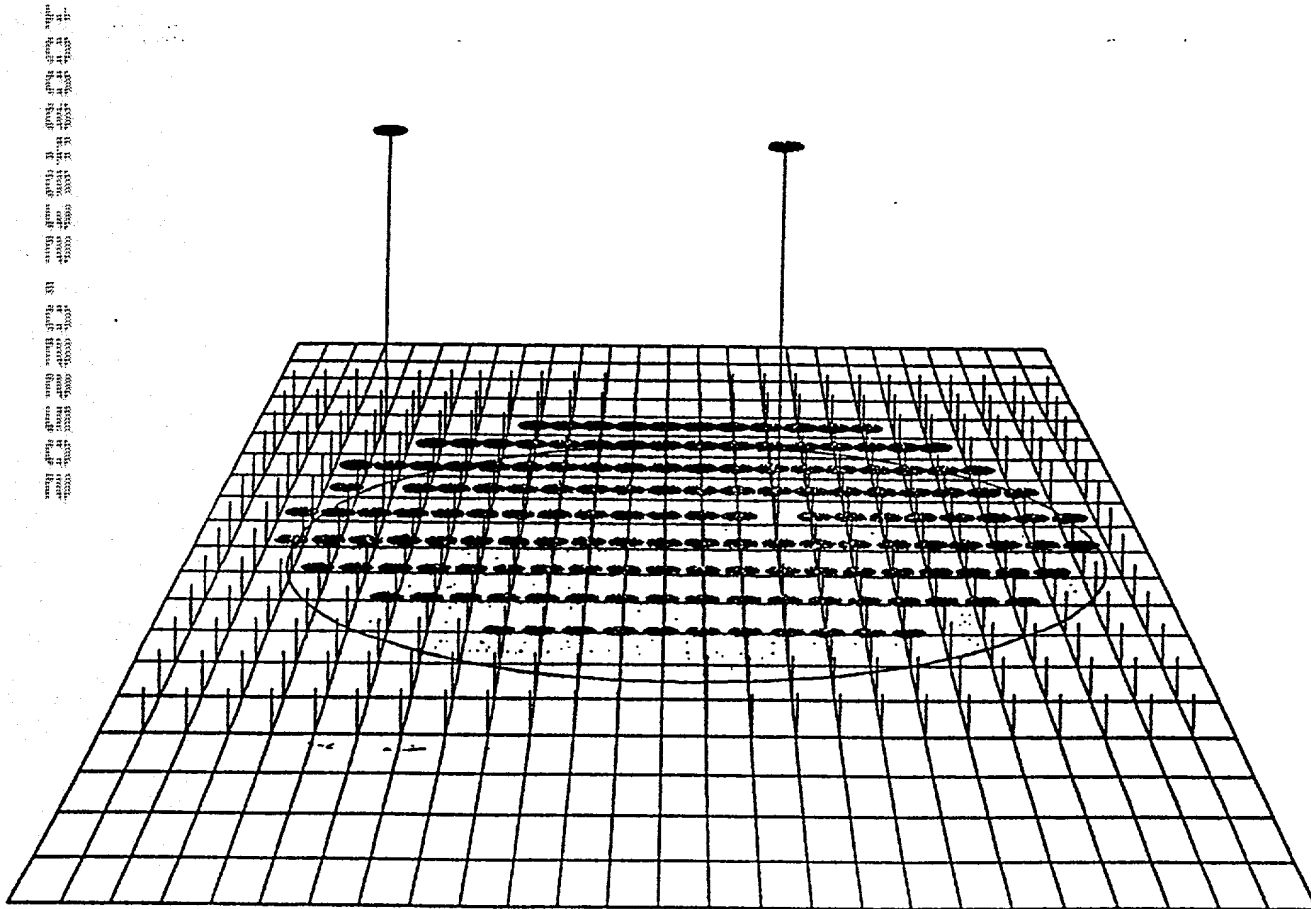


The disadvantage is that very small or very sparse binding events tend to be statistically reduced to insignificance when averaged over this relatively large spot area.


Figure 4 *OB*

New Microbiological Use

Determination of individual binding events or CFUs

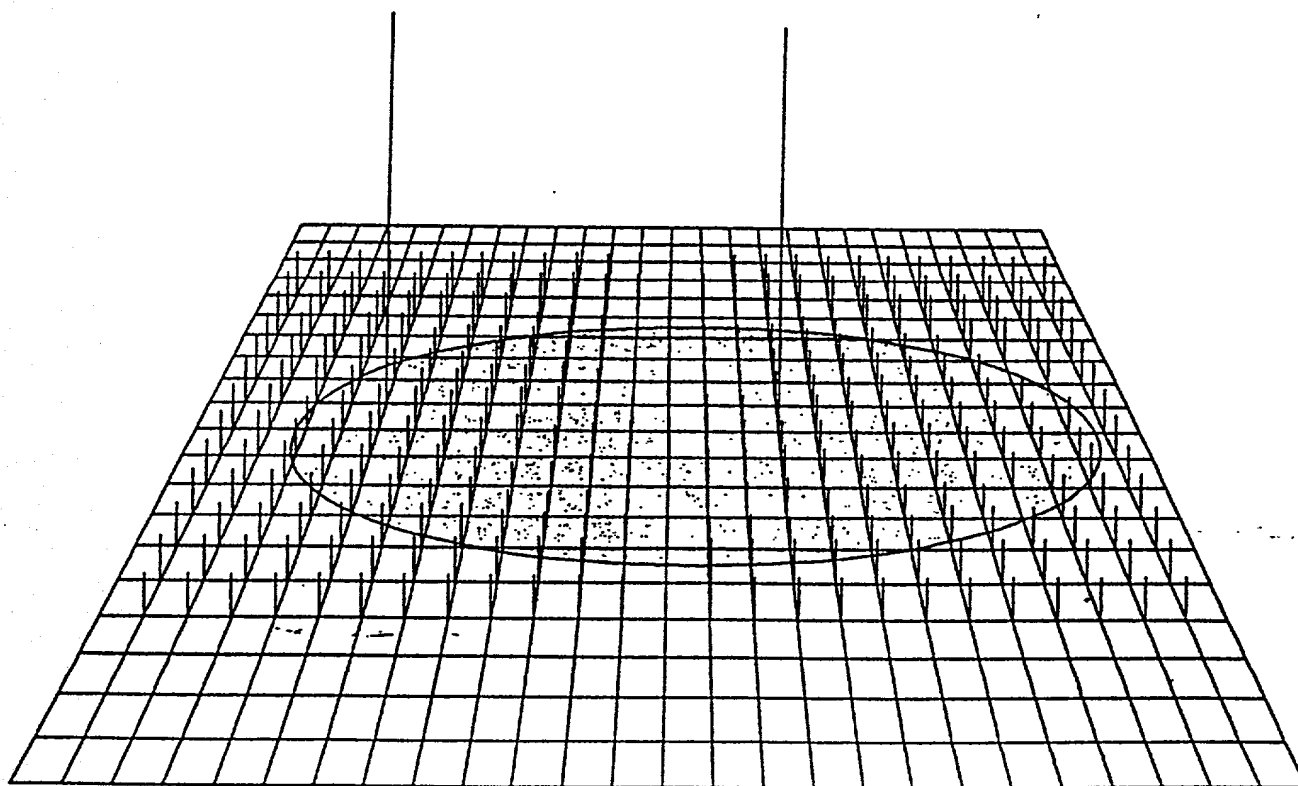


A scanning ellipsometric method or scatterometric method or both, when used with a very small beam diameter (in this case 20um) can provide a vastly higher relative signal for discrete binding events (that is as averaged over a much smaller spot area).

Figure 5 
mold - TS - 24077

New Microbiological Use

Determination of individual binding events or CFUs



This approach allows for the surface to be ~~measured~~^{resolved} as a type of topology. It is, in fact, because the binding events are not integrated over the surface that this method can be used to approximate individual or discrete binding event identification (depending upon the diameter of the beam used).

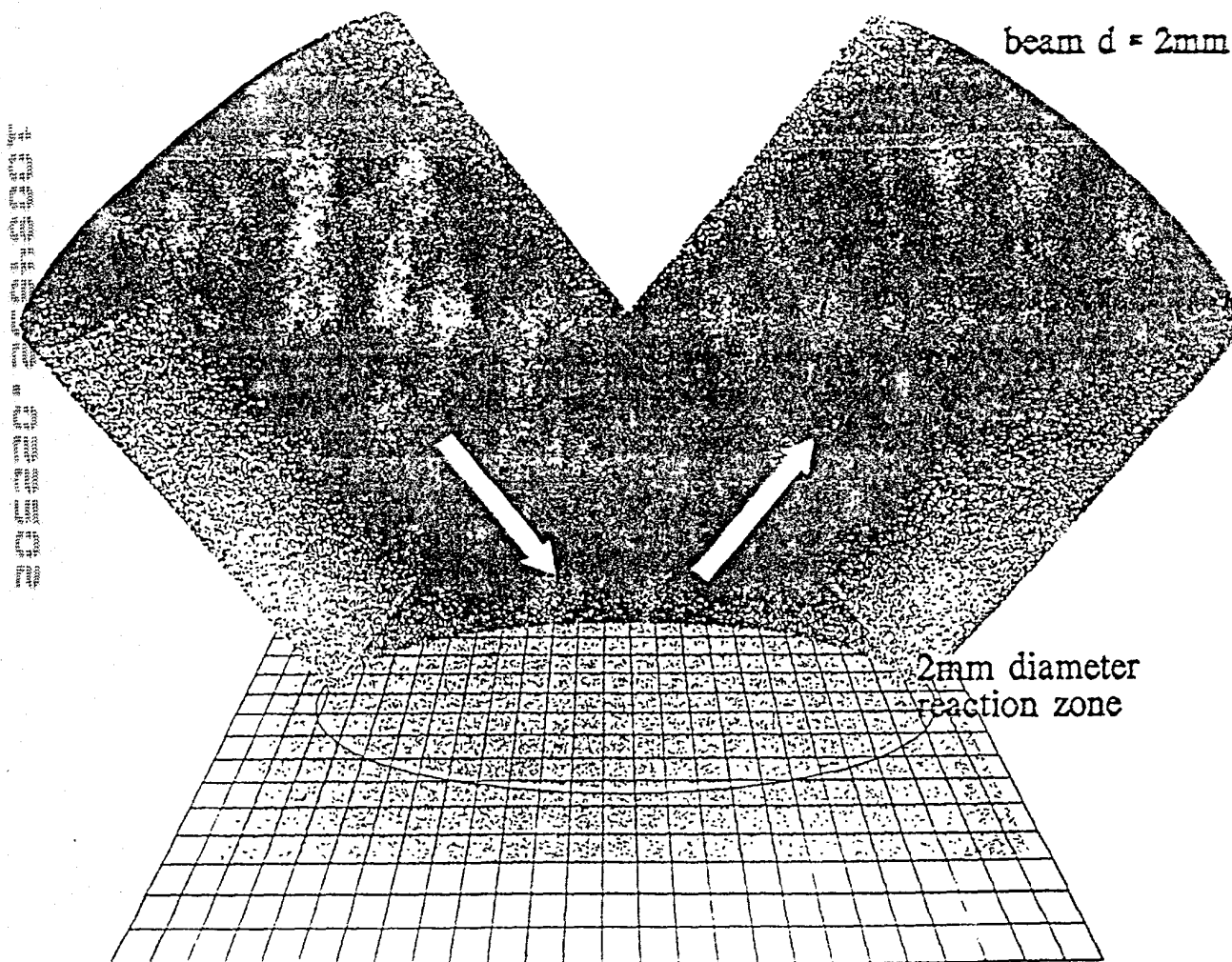
Figure 5 

Aggregate vs. Scanning Ellipsometry

Innovation Group

Current OTER Laser Configuration

Determination of aggregate response over the beam spot area



$$\pi \cdot r^2 = SA \text{ (in mm}^2\text{)} = 3.14159 \times 1^2 = 3.14159 \text{ mm}^2$$

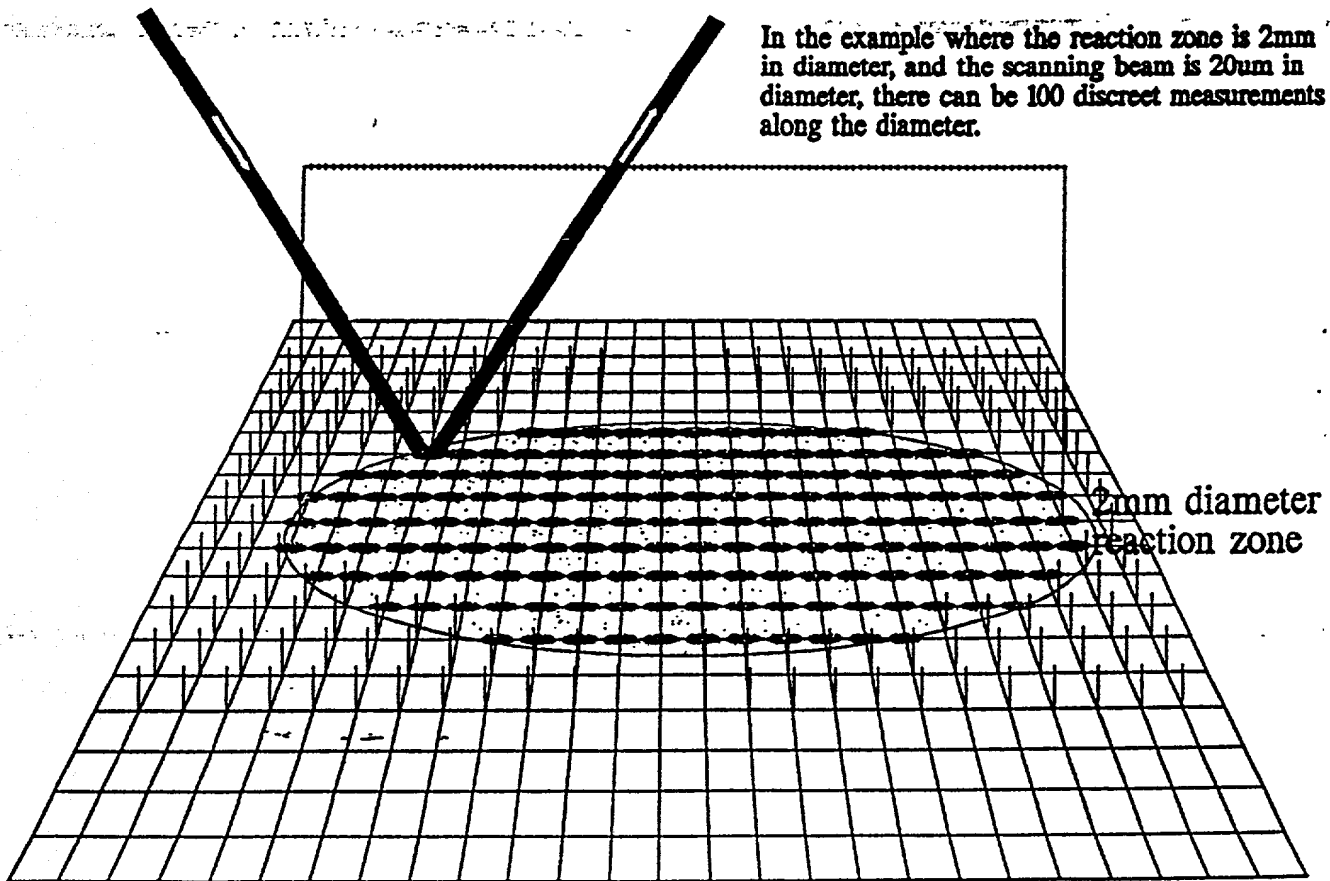
Figure 7 OB

mm2.pdf - 13 - 2007

Scanning Micro-Laser Configuration Determination of individual cellular-scale readings

For Example:
beam $d = 20\mu\text{m}$

In the example where the reaction zone is 2mm in diameter, and the scanning beam is 20 μm in diameter, there can be 100 discrete measurements along the diameter.



10,000 A = 1 μm

1,000 μm = 1mm

Angstrom Unit = 3.937×10^{-9} inch, 1×10^{-10} meters, 1×10^{-4} microns, 0.1 milli-micron (micro-millimeter).

Micron = 3.937×10^{-5} inch, 0.039370 mil, 1×10^{-6} meter, 0.001 millimeter, 1×10^4 Angstrom units.

$$1 \text{ mm}^2 = 1,000,000 \text{ } \mu\text{m}^2$$

$$\text{Reaction zone SA} = 3,141,590 \text{ } \mu\text{m}^2$$

$$\text{Scanning beam reads } 314.159 \text{ } \mu\text{m}^2$$

Thus a 20 μm beam can make 10,000 discrete readings within the reaction zone

Figure 8

ms2.pdf - 75 - 1/2/97

Aggregate vs. Scanning Ellipsometry

How Big is Small ?

In the case where a single organism ($1 \mu\text{m}^3$) is to be measured on a 2 mm^2 surface:

$$\frac{314,159,000,000 \text{ A}^2 \text{ surface area of spot}}{78,500,000 \text{ A}^2 \text{ surface area of organism}} \longrightarrow \text{ratio of } 4,000,000 \text{ A}^2 : 1 \text{ A}^2$$

$10,000 \text{ A (height)} / 4,000,000 = 0.00250 \text{ A (height) contribution across the spot}$

$$1 \times 10^2 \text{ cells} / .02 \text{ ml} = 5 \times 10^3 \text{ cells} / \text{ml} \longrightarrow 25 \text{ A (height) contribution across the spot}$$

$$1 \times 10^3 \text{ cells} / .02 \text{ ml} = 5 \times 10^4 \text{ cells} / \text{ml} \longrightarrow 25 \text{ A (height) contribution across the spot}$$

$$1 \times 10^4 \text{ cells} / .02 \text{ ml} = 5 \times 10^5 \text{ cells} / \text{ml} \longrightarrow 25 \text{ A (height) contribution across the spot}$$

$$1 \times 10^5 \text{ cells} / .02 \text{ ml} = 5 \times 10^6 \text{ cells} / \text{ml} \longrightarrow 250 \text{ A (height) contribution across the spot}$$

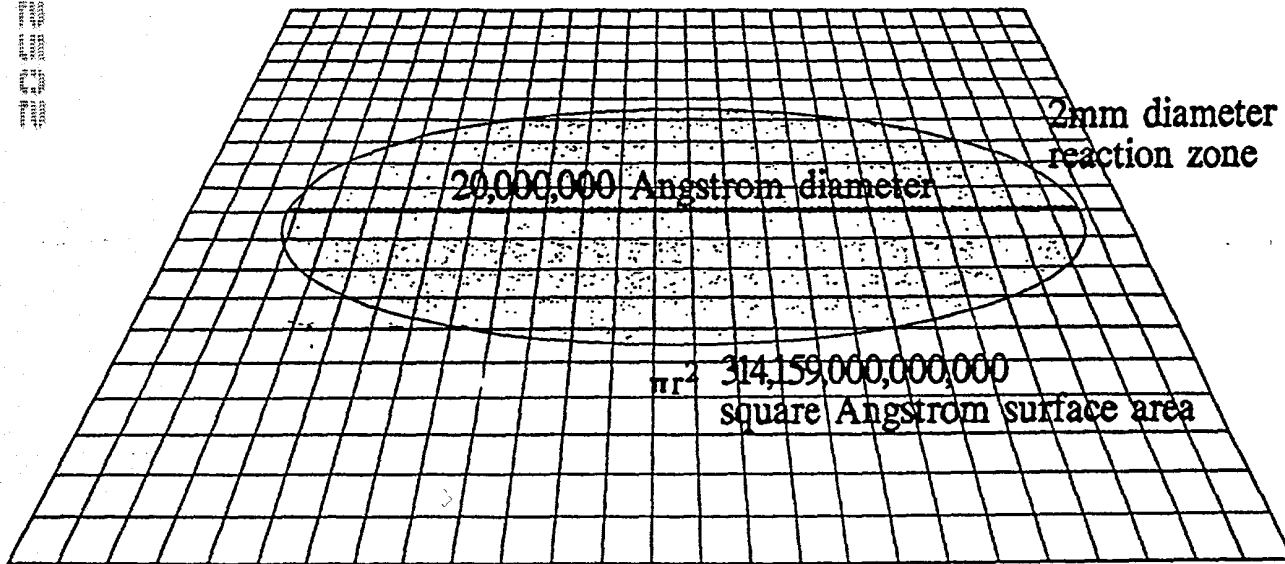
$$1 \times 10^6 \text{ cells} / .02 \text{ ml} = 5 \times 10^7 \text{ cells} / \text{ml} \longrightarrow 2500 \text{ A (height) contribution across the spot}$$

probable unamplified
detectability limit

With an amplification system that provided 2X mass, the system needs 2.5×10^6 cells / ml

With an amplification system that provided 5X mass, the system needs 1×10^6 cells / ml

With an amplification system that provided 10X mass, the system needs 5×10^5 cells / ml



$10,000 \text{ A} = 1 \mu\text{m}$

$1,000 \mu\text{m} = 1 \text{ mm}$

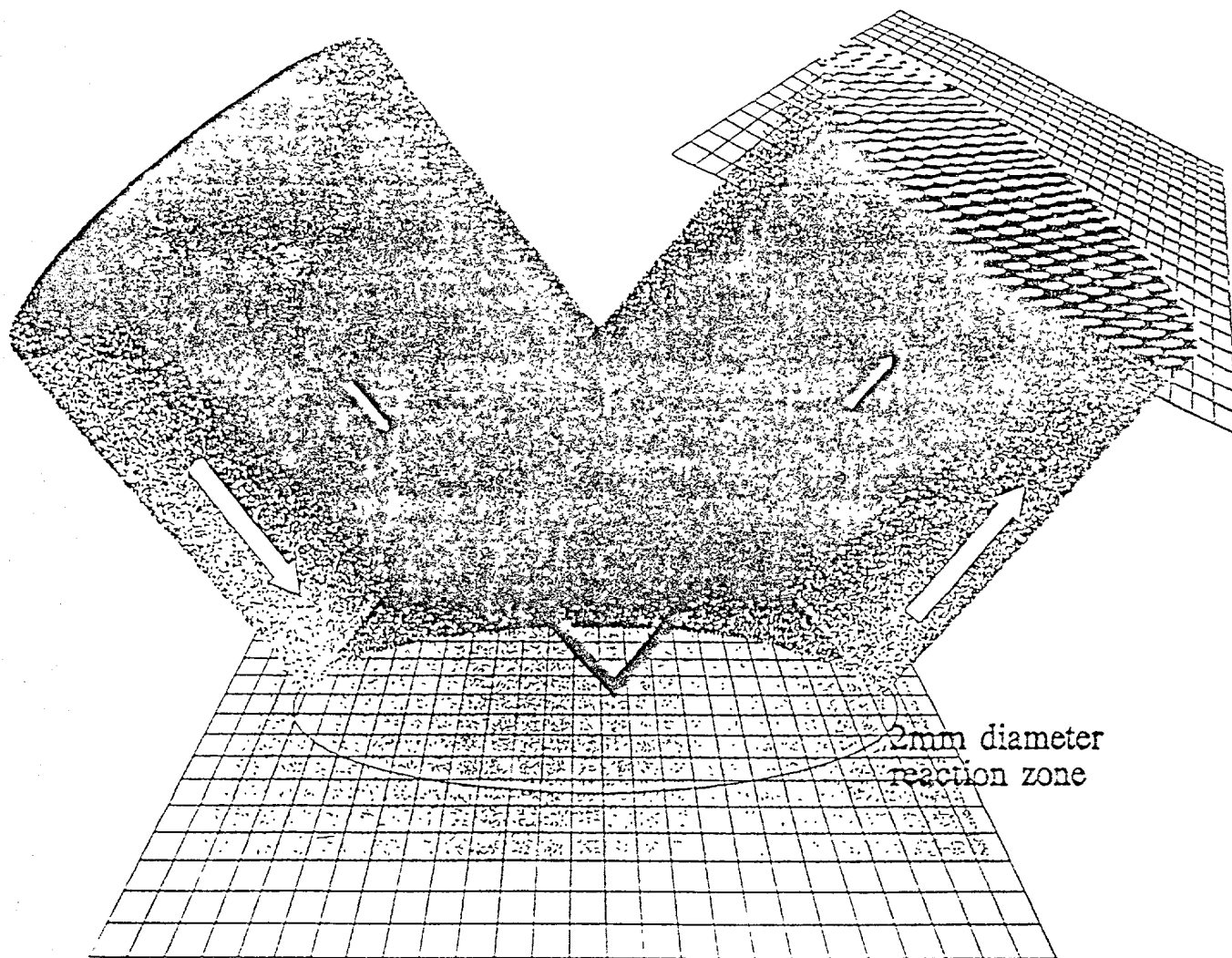
Angstrom Unit = 3.937×10^{-9} inch, 1×10^{-10} meters, 1×10^{-4} microns, 0.1 milli-micron (micro-millimeter).

Micron = 3.937×10^{-5} inch, 0.039370 mil, 1×10^{-6} meter, 0.001 millimeter, 1×10^4 Angstrom units.

Figure 9  2nd ed. - 73 - 1007

An alternative to the small beam "Scanning" approach is the use of a CCD or diode array to read and "parce" the larger laser beam into smaller discrete signals.

Determination of small spot response within the large beam spot area

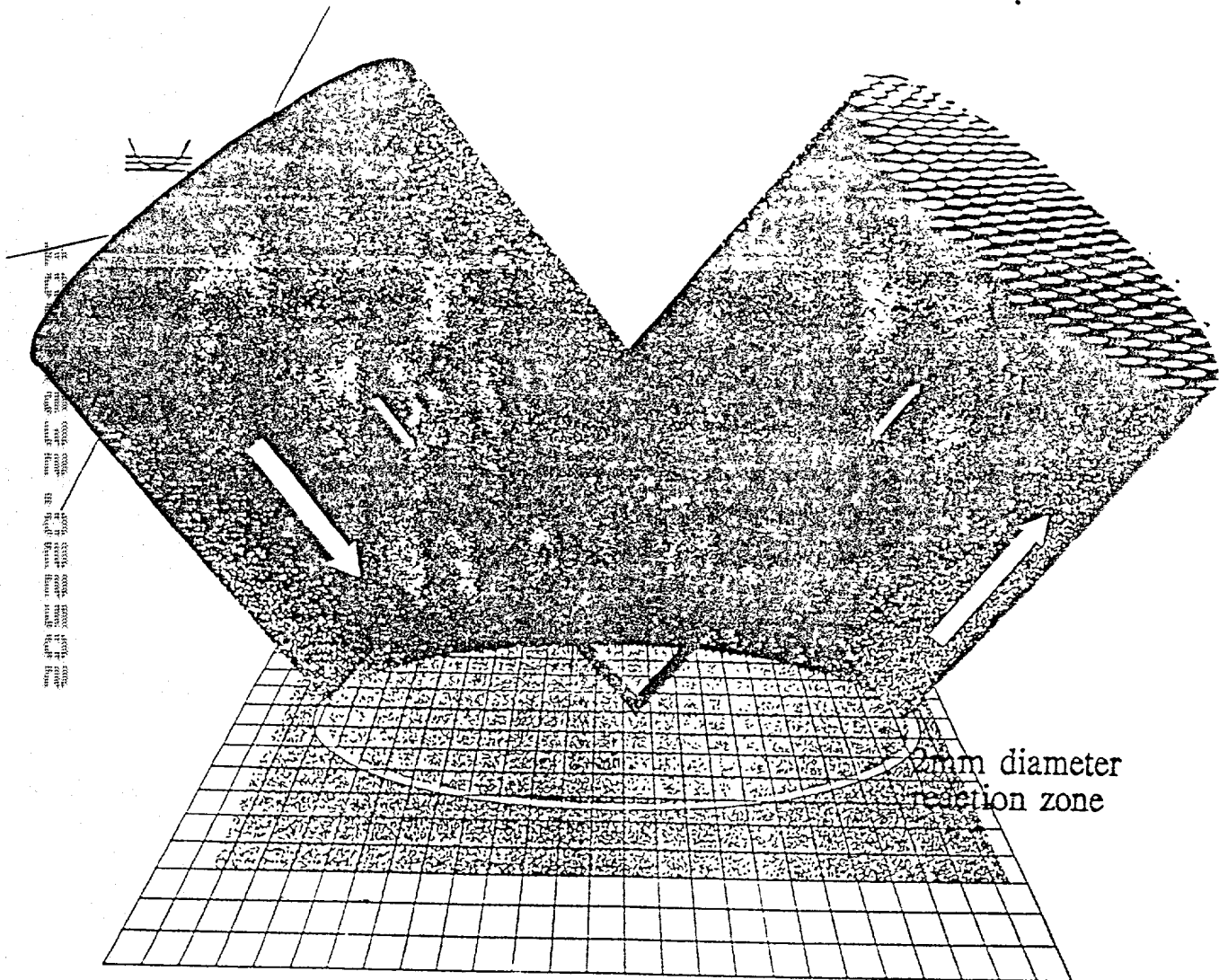


This effectively creates a "virtual" beam (defined by the path that the light intersecting the array at a specific dection point has taken).

The aggregate signal for all virtual beams equals the large beam signal, but each virtual beam references only a limited surface area. The virtual beam approach may be subject to greater error than the small beam approach, due in part to the potential for signal mixing across the array, however it allows for a major increase in sensitivity over the large beam approach.

Figure 10 *[Signature]* - 13 - 8/2/77

The specific optical signal can be selected so as to provide the appropriate level of information, based upon the nature or the material to be detected, and the resolution desired.



A variety of optical signals may be used within this system.

The examples provided in this discussion use ellipsometry as the example optical method. However it is expected that a variety of optical methods will be substantially improved by adopting the general approach described here. In particular we have demonstrated that scattering methods will form the basis of one class of instruments that is distinct from ellipsometry. Other effects such as absorption, refractive index change, chiral effects, and diffraction may be used within an essentially similar optical configuration, and may provide particular and significant benefits.

Figure 11  1000-1-1-10/2/97


Principle	Label Type	Instrument	DDx Status
Scatter	polymer beads/particles silica beads/particles magnetic beads/particles metal beads/particles metal coated beads/particles	scatterometry	demonstrated
Optical absorption	colloidal gold magnetic beads	reflectometry photometry	scheduled
Change in polarization state	polymer beads silica beads	ellipsometry (with compensator) polarimetry (wout compensator)	scheduled
Change in refractive index	high refractive index or optically active materials	ellipsometry (with compensator) polarimetry (wout compensator)	scheduled
Chiral effects	azio dyes chiral compounds		envisioned
Diffraction effects	patterned surface	interferometry	envisioned
Spectroscopic effects	wavelength selective materials	spectrometer	envisioned

Signal reception techniques might include:

single diode detector - e.g. scanning (small beam method)

diode array detector - e.g. array (virtual beam method)

CCD detector - e.g. array (virtual beam method)

Figure 12 
msd.gpl - 73 - 2/13/97

For either the Scanning (small beam) or the Array (virtual beam) approach, a substantial improvement in signal delectability may be possible by using unique characteristics of optically based mass detection systems.

Properties of the mass enhancement label may alter the optical signal due to a number of physical characteristics, including:

- refractive index
- scatter
- chiral effect
- general adsorption
- wavelength specific adsorption
- diffraction

*} should be absorbance
What's the difference between these two?*

effectively creating an improved ability to discriminate the signal generated by the binding of the label to the complex from that created by surface background or in the absence of specific binding events. This may operate through the creation of an enhanced or attenuated "apparent" signal over that which would be created by "normal" materials.

Scale of normal vs. optically active elements @ 2X effect

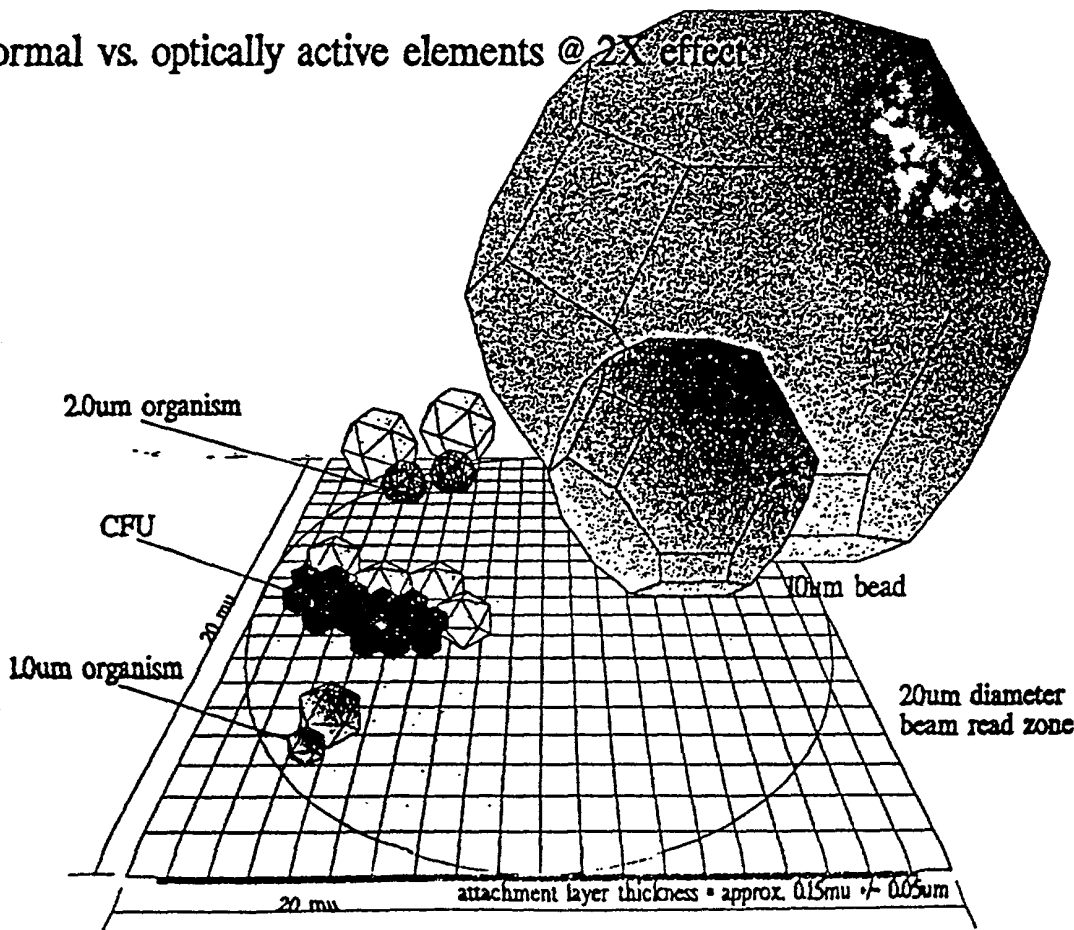


Figure 14 *[Signature]* TM - 14097

15/15

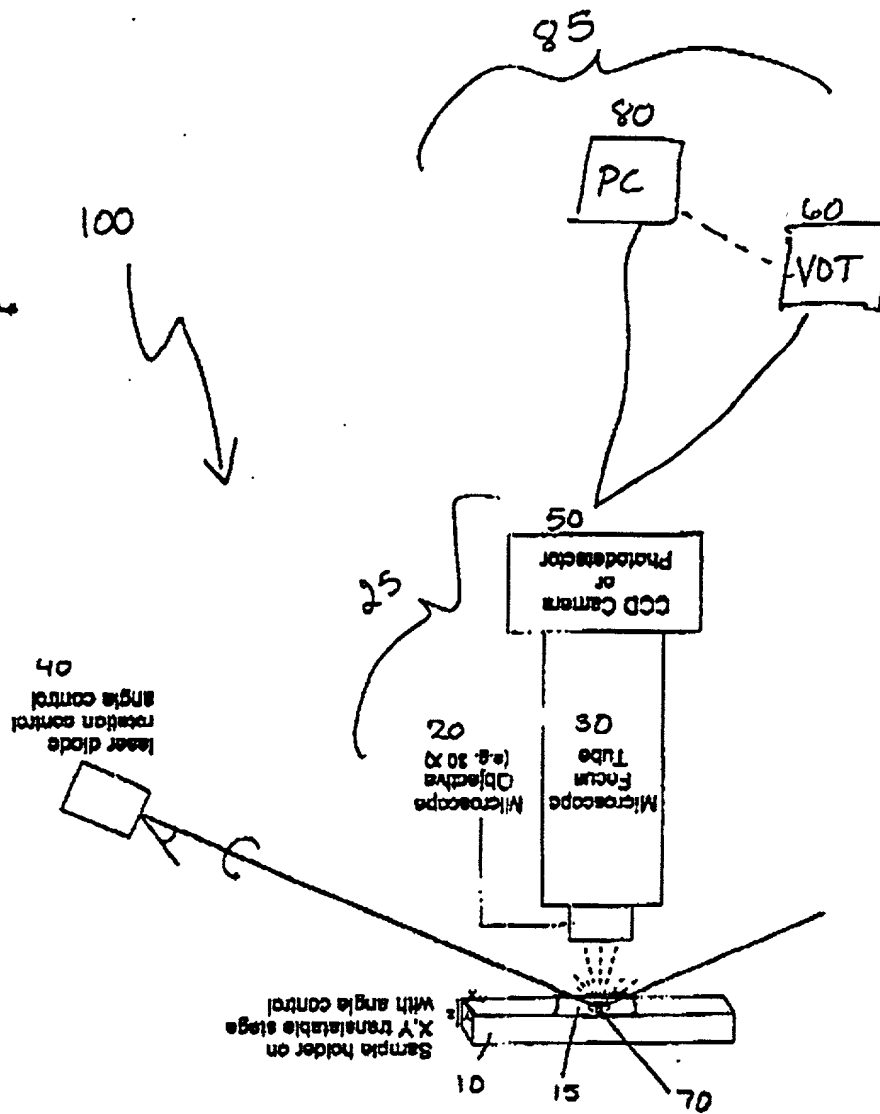


Fig. 15

500L REPRODUCIBLE LOGIC CONF MAY-88-97 03:07PM FROM 203130071+203 040 1047 PAGE 17 1

26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

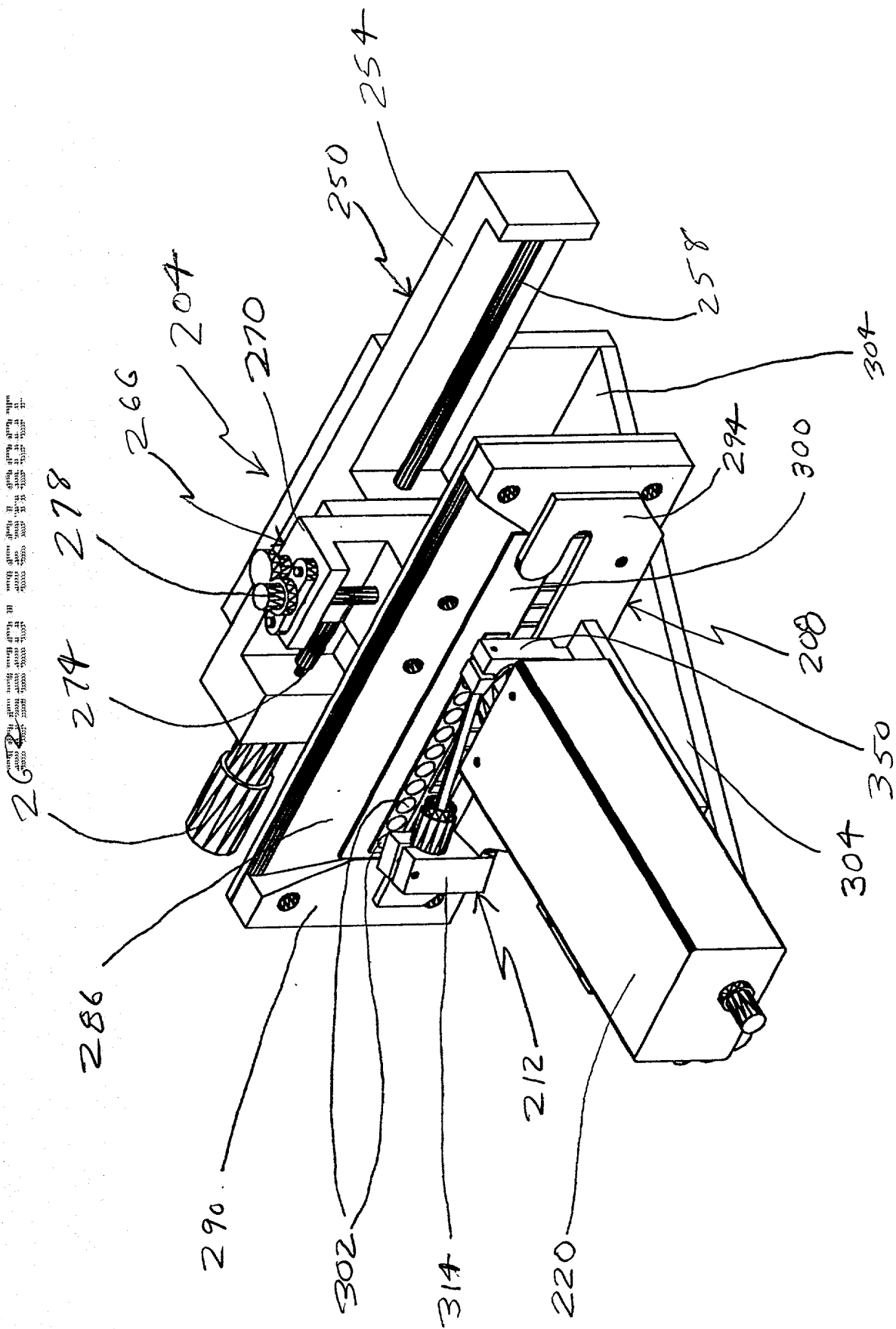
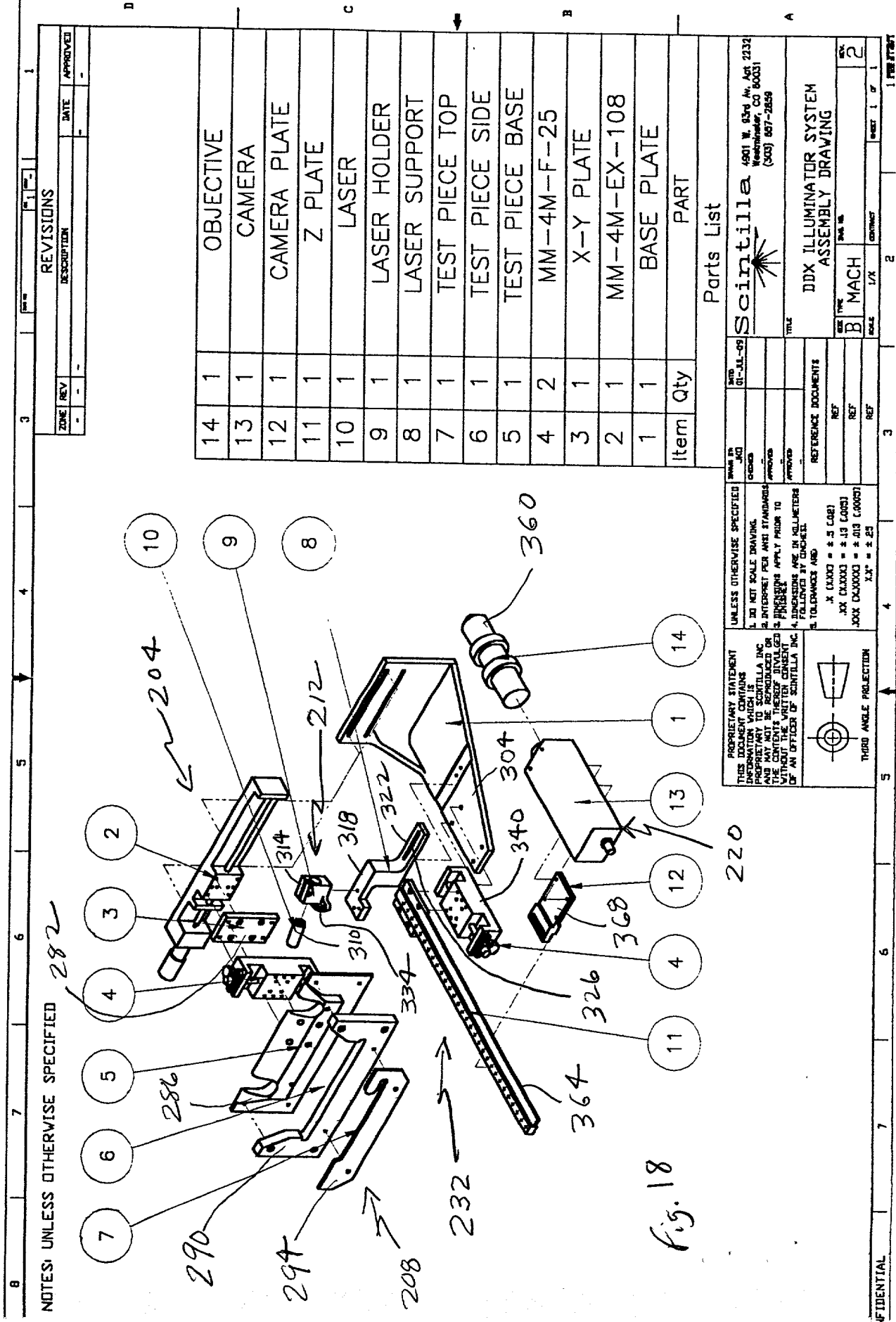


Fig. 17



8	7	6	5	4	3
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REVISIONS					
ZONE		REV	DESCRIPTION	DATE	APPROVED
		-		-	-

NOTES: UNLESS OTHERWISE SPECIFIED

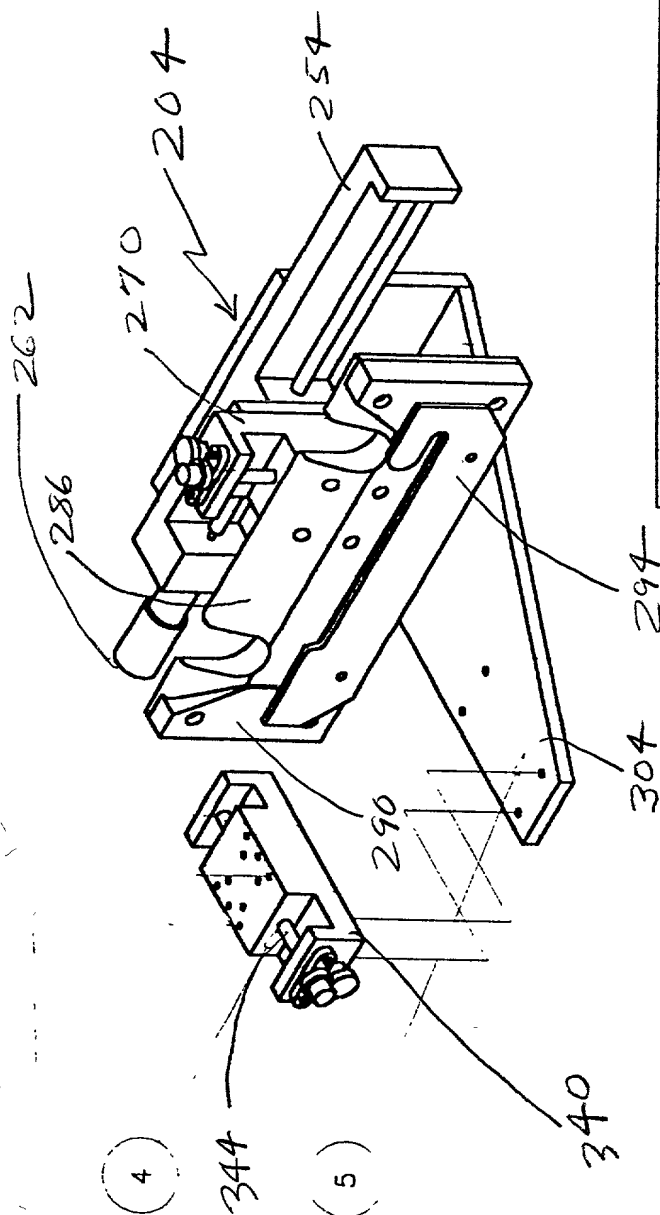



Fig. 19

Item	Qty	Name
5	5	FORTH ASSEMBLY
4	4	MM-4M-F-25
3	3	Z-PLATE
2	2	LENS CELL HOLDER
1	1	LASER HOLDER

PARTS LIST		DRAWN BY JAC		DATE 04-JUN-61		TITLE DDX ILLUMINATOR SYSTEM FORTH MECHANICAL ASSEMBLY		4901 W. 34th Av. Apt 2232 Northridge, CA 90031 (805) 837-2859		PART 1 OF 1	
UNLESS OTHERWISE SPECIFIED		APPROVED		SCALE 1/4"		SHEET NO. 1		SCINTILLA		SHEET	
1. 10 NOT SCALE DRAWING.		APPROVED		REFERENCE DOCUMENTS		REF		REF		REF	
2. INTERSECT PER ANG STAGNATIONS		APPROVED		REF		REF		REF		REF	
3. DIMENSIONS APPLY PRIOR TO FINISHES		APPROVED		REF		REF		REF		REF	
4. DIMENSIONS ARE IN MILLIMETERS FOLLOWED BY DECIMAL		APPROVED		REF		REF		REF		REF	
5. TOLERANCES ARE: .X DIM. = ± .5 (.02) .XX DIM. = ± .13 (.013) .XXX DIM. = ± .013 (.0013) .XXY = ± .25		APPROVED		REF		REF		REF		REF	
PROPRIETARY STATEMENT THIS DOCUMENT CONTAINS INFORMATION WHICH IS PROPRIETARY TO SCINTILLA INC. AND ANY NOT BE REPRODUCED OR TRANSMITTED IN ANY FORM OR BY ANY MEANS, ELECTRONIC OR MECHANICAL, WITHOUT THE WRITTEN CONSENT OF AN OFFICER OF SCINTILLA INC.		APPROVED		REF		REF		REF		REF	
		APPROVED		REF		REF		REF		REF	
THIRD ANGLE PROJECTION		APPROVED		REF		REF		REF		REF	

OPTICAL BENCH. LIGHT RAYS ARE MODELED IN THIS RENDERING. THE LASER IS SHOWN AT THE NOMINAL 13.5° FROM THE TEST PEICE. IT IS ADJUSTABLE FROM 4.5-34.5°. THE LASER AND LENS CELL HOLDERS ARE C-CLAMPS. THEY WILL BE MACHINED SUCH THAT A SET SCREW IS NOT NEEDED, BUT IN THE FUTURE IT MAY BE NEEDED SO THE SET SCREW WILL BE MACHINED NOW (AS SHOWN). THE LENS CELL HAS ADJUSTABILITY VERTICAL TO THE TEST PEICE WITH STRAIGHT PIN-N-SLOT & ONE RETENTION SCREW IN THE SAME MANNER AS THE LASER HAS ROTATIONAL ADJUSTABILITY.

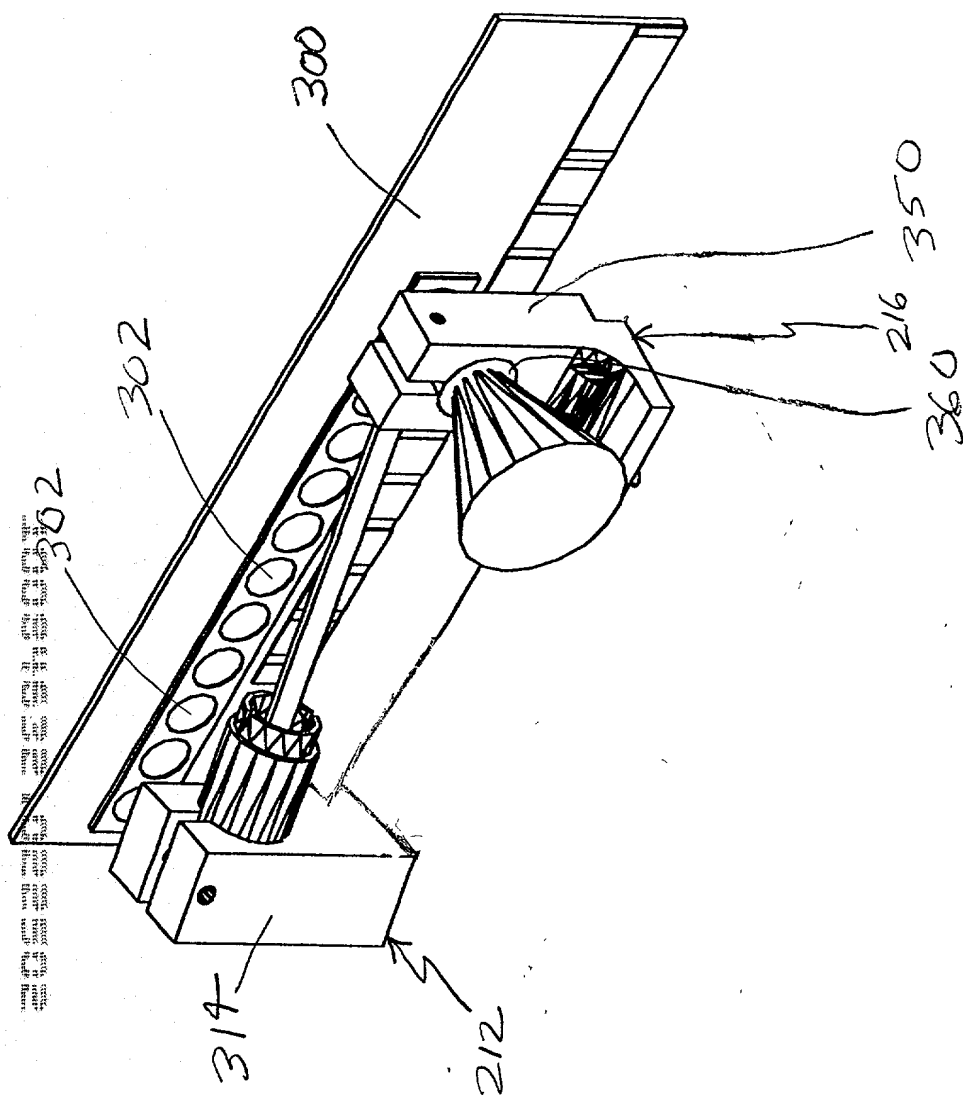


Fig. 20

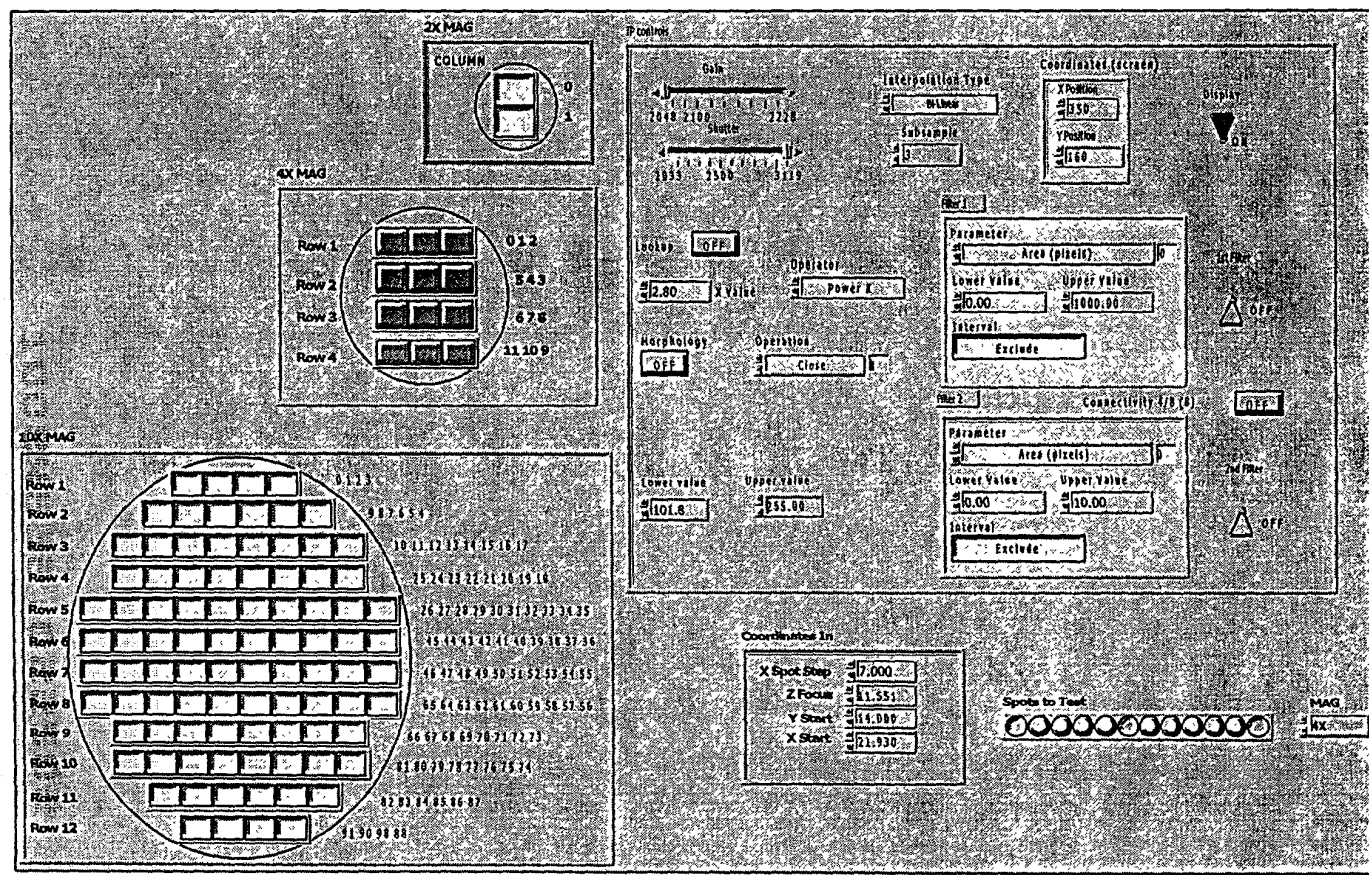
Write Profile.vi

D:\Data\Projects\Accelr8 DDx Optest\Programming\QuanDx10-28-01.IIb\Write Profile.vi

Last modified on 10/29/2001 at 12:59 PM

Printed on 11/15/2001 at 1:09 AM

Front Panel



Controls and Indicators

MAG

2X MAG

COLUMN

Boolean

4X MAG

Row 1

Boolean

Row 2

Boolean

Row 3

Boolean

Row 4

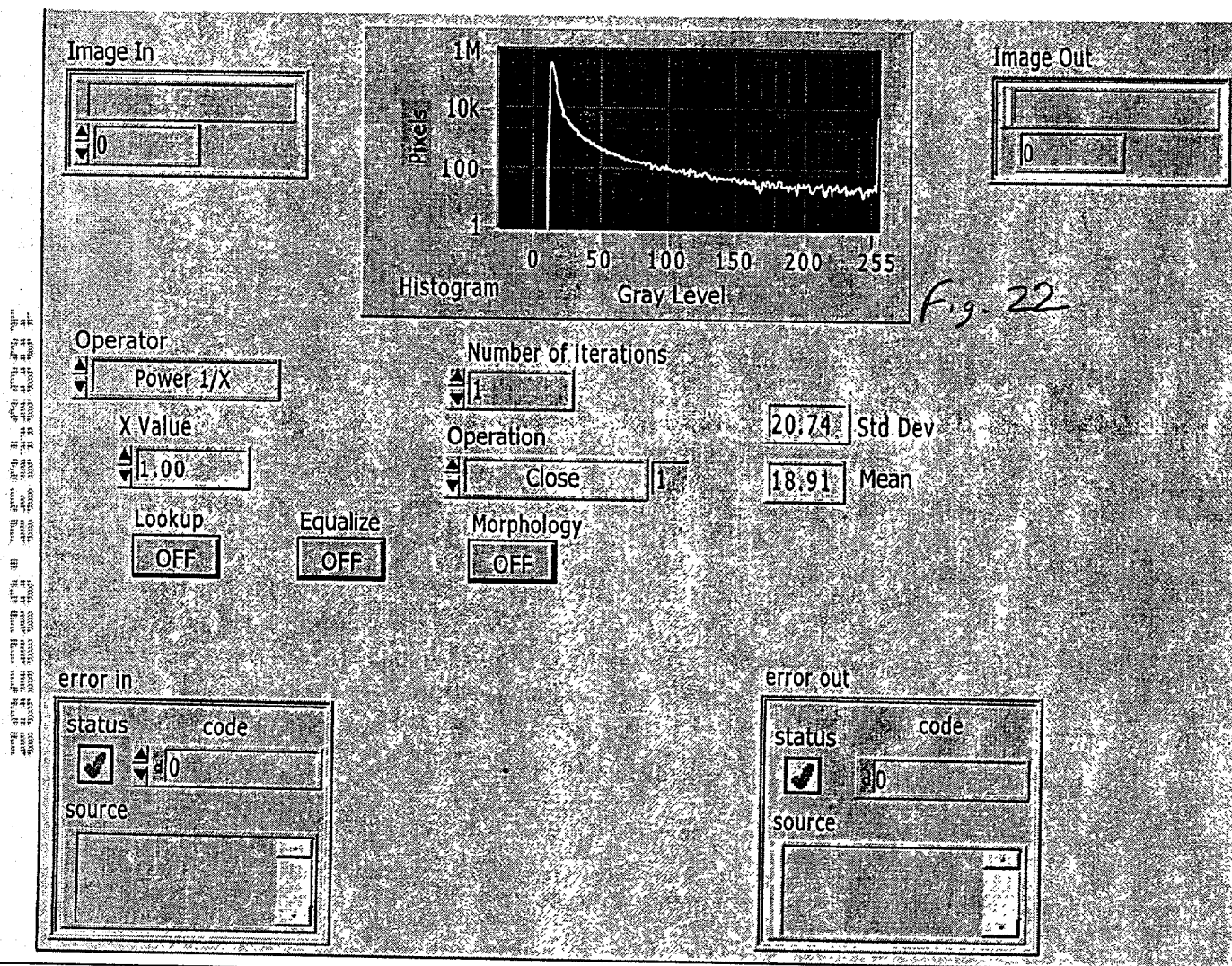
Boolean

10X MAG

Row 1

Fig. 21

Front Panel



Controls and Indicators

Operator

Operator specifies the remapping procedure used.

X Value

X Value is a value used only for the operators Power X and Power 1/X.

Equalize

Operation

Operation specifies the type of morphological transformation procedure to use.

Lookup

error in

The **error in** cluster can accept error information wired from VIs previously called. Use this information to decide if any functionality should be bypassed in the event of errors from other VIs.

The pop-up option **Explain Error** (or Explain Warning) gives more information about the error displayed.

INSTRUMENT SETUP

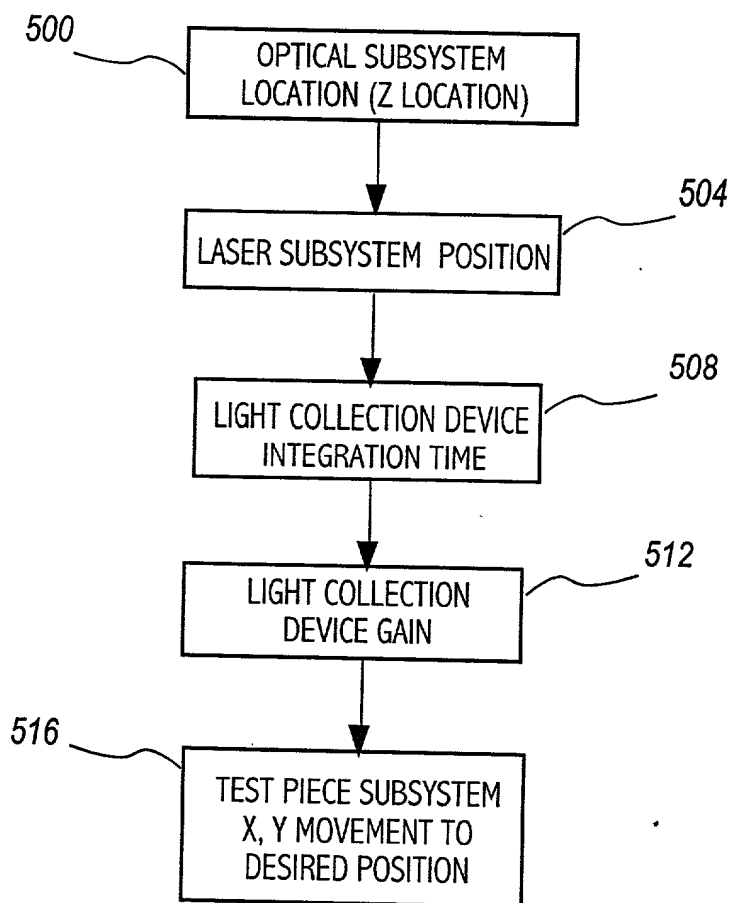


Fig. 23

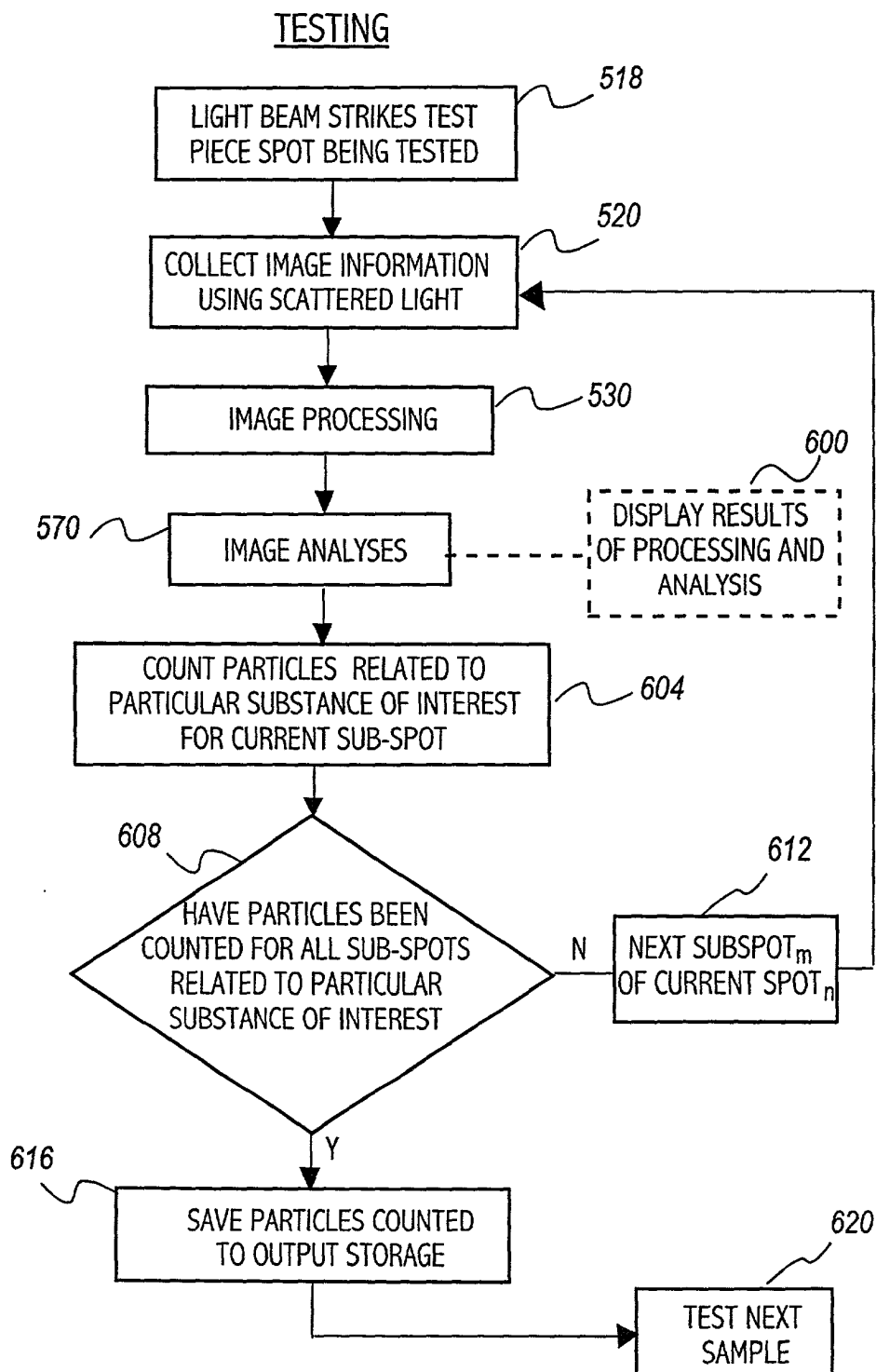


Fig. 24

IMAGE PROCESSING

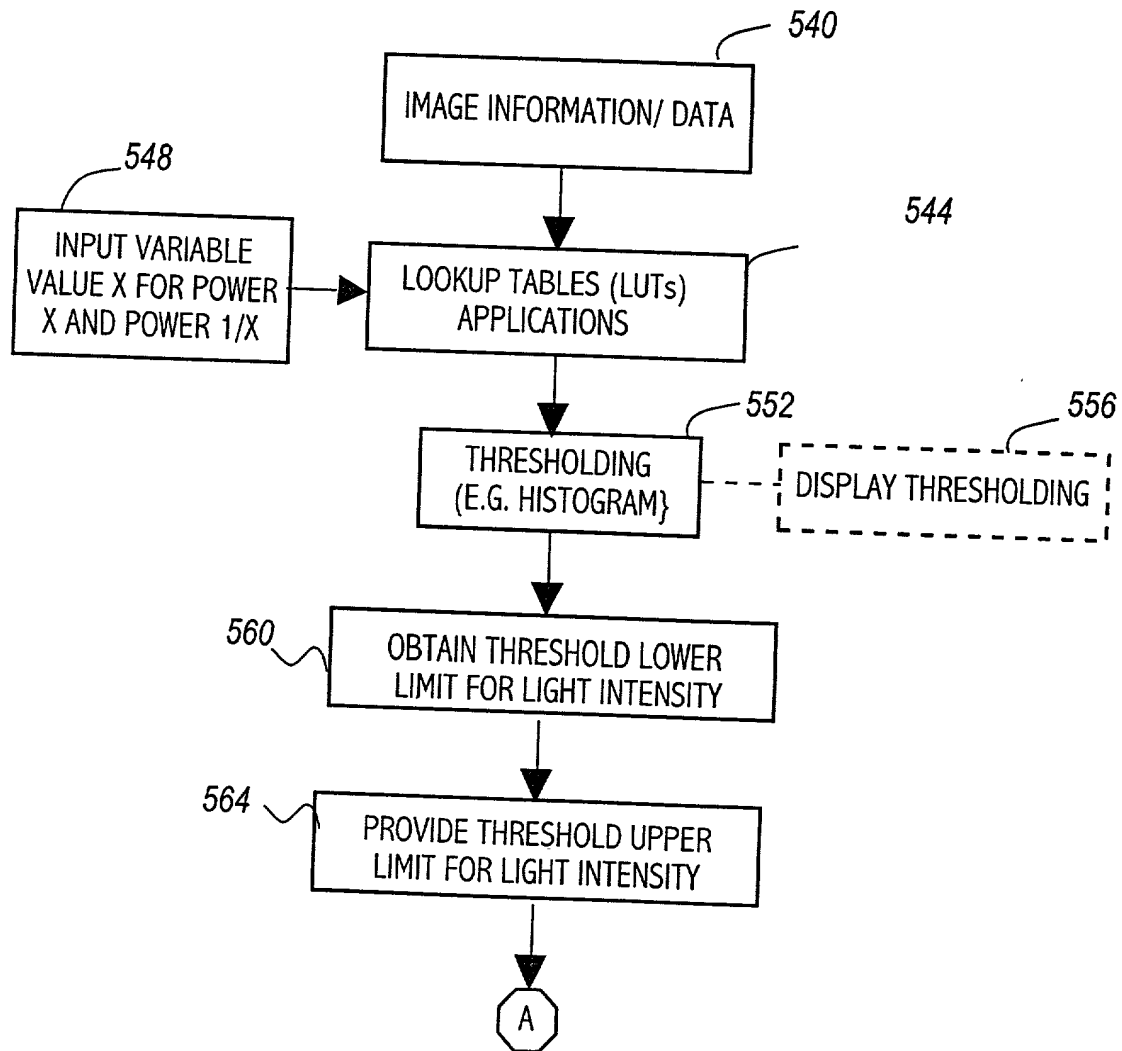


Fig. 25

IMAGE ANALYSIS

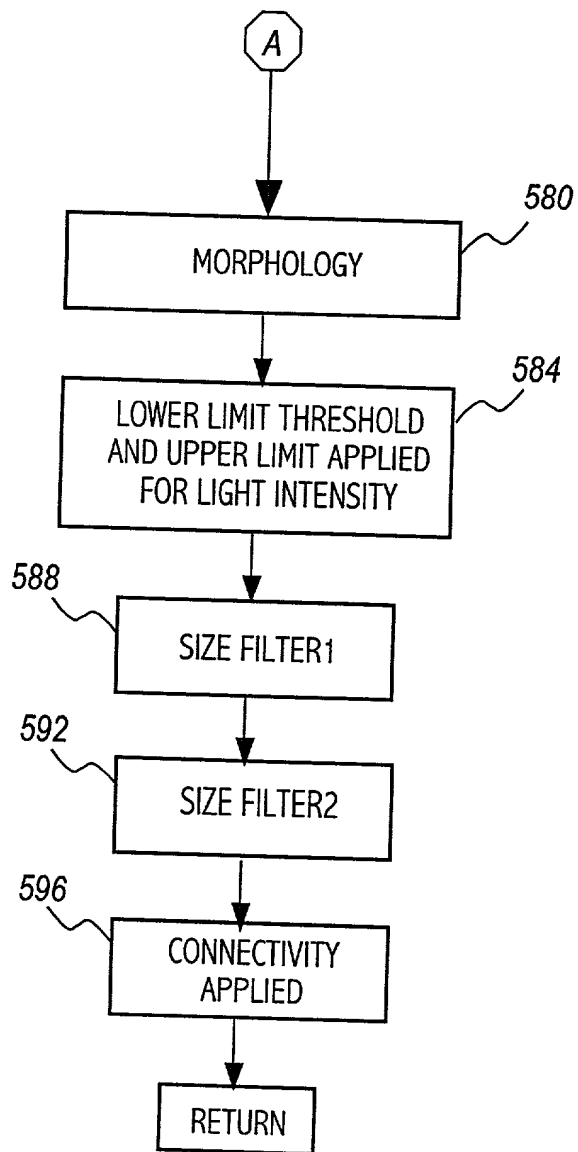


Fig. 26